Amendments To The Specification:

Please amend the sentence beginning at page 3, line 7 as follows:

Fig. 3 is cross-section view of the exhaust diffuser assembly shown in Fig. 2, taken along cutting plane 3-3~~III-III~~' therein

Please amend the sentence beginning at page 6, line 1 as follows:

As seen with reference to Figure 4~~5~~, working fluid 18 leaving the engine turbine section 14 is characterized by a first velocity profile 38 upon entering the flowpath first region 32 and a second velocity profile 40 upon leaving the second region 34. The second velocity profile 40 is generated by the flow deflecting member 36 as the working fluid 18 flows through the flowpath first region 32 and into the flowpath second region 34. With continued reference to Figure 2, and with additional reference to Figures 3 and 4, the flow deflecting member 36 encircles the inner boundary sleeve 22 and resembles a tapered ring that includes an upstream-facing guide surface 56. The guide surface 56 is oriented to direct working fluid 18 into a desired course within the flowpath second region 34. As seen with particular reference to Figure 4, the guide surface 56 is substantially linear and is characterized by three defining dimensions: a surface length L_{gs}, a deflection angle α, and an outer radius r_{ogs}. The surface length L_{gs} is the distance from the distal end of the guide surface 56 to the inner boundary sleeve 22; the deflection angle α is measured between the central axis 24 and the guide surface 56; and the outer radius r_{ogs} is the distance between the central axis 24 and the radially-outward end of the guide surface. It has been determined that the flow deflecting member 36 functions best when the guide surface 56 deflection angle α lies below about forty-five degrees. Additionally, to allow appropriate working fluid 18 divergence within the flowpath first conditioning zone 42, the flow deflecting member 36 is axially positioned within the second conditioning zone 44, and more particularly, along the inner boundary sleeve second portion 54. Other axial locations may be used if fluid divergence is not critical.

Please amend the paragraph beginning at page 7, line 3 as follows:

With continued reference to Figure 4~~5~~, this radial distribution is generated when the guide surface outer radius r_{ogs} is no larger than the outer radius r_{oib} of the inner boundary sleeve 22 in the inner boundary first portion 50. As noted above, the deflection angle α provides optimal

performance when below about forty-five degrees, and the defining dimensions are interrelated; therefore, once outer radius $r_{o\underline{gs}\cancel{dm}}$ is selected, the appropriate surface length $L_{\underline{gs}\cancel{dm}}$ is a matter of geometry, with the appropriate length generating a guide surface 56 having a desired outer radius $r_{\cancel{e}iob}$ and a deflection angle α of about forty-five degrees.

Please amend the paragraph beginning at page 7, line 11 as follows:

Other flow profiles may be produced. For example, it may be desired in some cases to direct a higher concentration of heat toward the outer boundary sleeve. In instances where an associated HRSG 12' has been exposed to center-peaked, or "hub-strong" concentrations of heat for extended periods of time, it may be desirable to direct heat away from previously-damaged, radially-inward HRSG regions. As will be discussed further below, it is also possible to ensure a uniformly-distributed velocity profiles and outwardly-biased velocity profiles, as well. In engines 16 that do not have HRSGs 12, it would still be advantageous to not have hot spots in the center portion of the exhaust ducting down stream of the diffuser section of the engine, for example in settings where plant ducting (not shown) makes a turn and centrally-located hot spots might damage the associated turning elbow (not shown). In such instances, the outer radius $r_{o\underline{gs}\cancel{dm}}$ is, as shown in Figure 6, selected to be larger than the outer radius $r_{\cancel{e}iob}$ of the inner boundary sleeve 22. It is noted that the outer radius $r_{o\underline{gs}\cancel{dm}}$ need not be larger than the radius $r_{\cancel{e}iob}$ of the inner boundary sleeve 22 in order to deflect the flow outward. The appropriate surface length $L_{\underline{gs}\cancel{dm}}$ is again a matter of geometry, with the appropriate length generating a guide surface 56' having a desired outer radius $r_{\cancel{e}iob}$ and a deflection angle α of about forty-five degrees. This profile 40', while not necessarily maximizing energy extraction, will extend the useable life of a heat-stressed HRSG 12' by diverting heat away from damaged regions.